

# Consequences of EC 5 for Danish best practise

Jørgen Munch-Andersen  
Danish Timber Information

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- Most strength parameters should be declared in the CE-mark in accordance with prEN14592
- Eurocode 5 equations can be used where applicable, but Initial Type Testing (ITT) is needed for many types of fasteners
- Eurocode 5 ought to give slightly conservative parameters

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- Embedment strength not a declared parameter

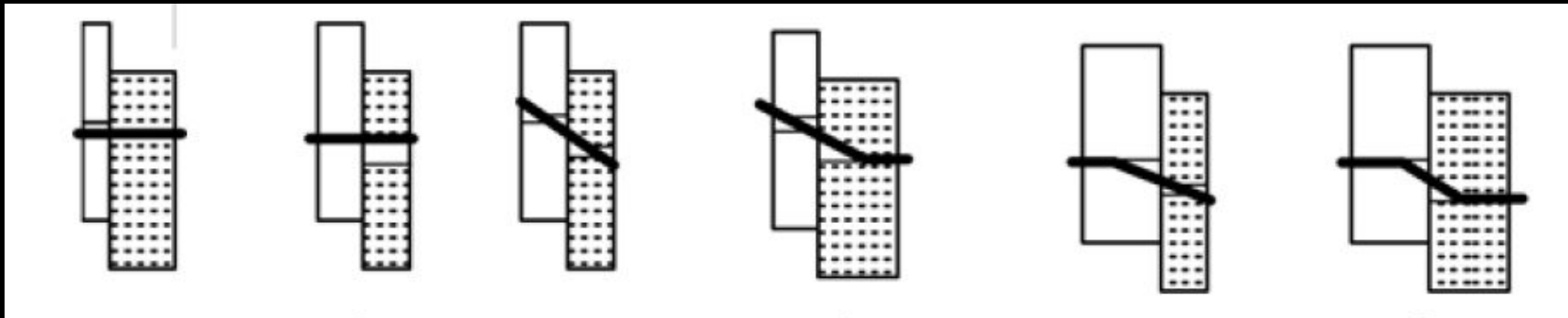
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- ITT not yet carried out for relevant fastener types
- Embedment strength not a declared parameter
- Load capacity for fasteners generally decreases
- Some common Danish connection types can no longer be used

# Strength parameters

Dowel ( $F_{\text{Johansen}}$ ): combination of

- Embedment strength of timber – depends on density
- Yield moment of dowel – depends on steel strength

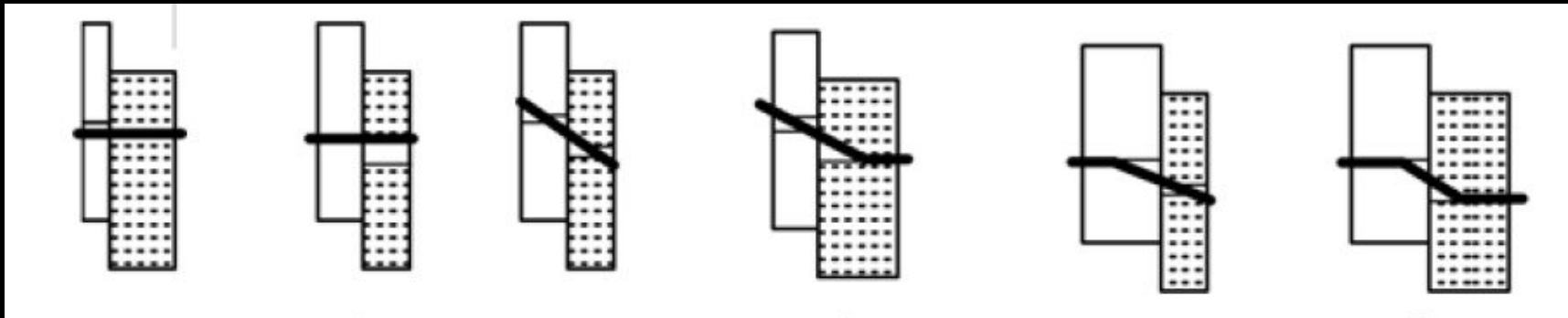




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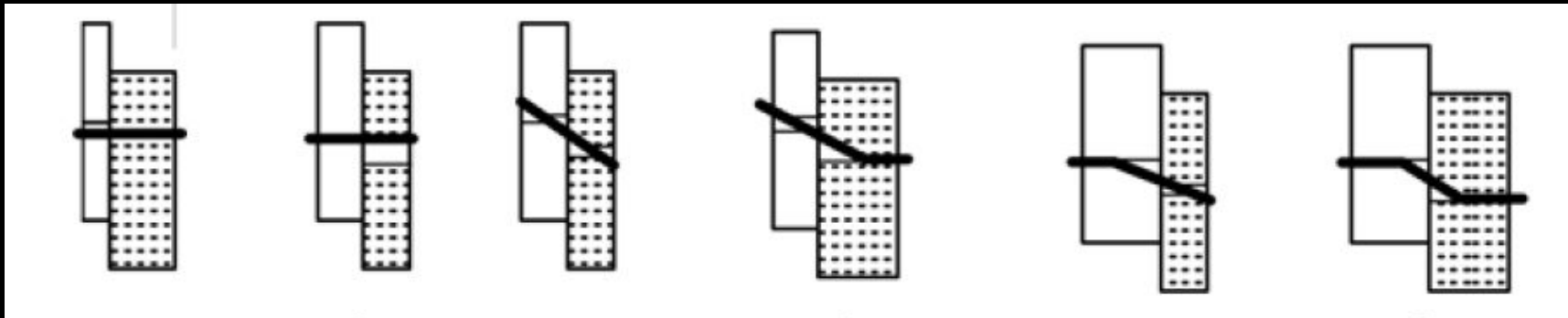
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Lateral load

- Combination of dowel and tension
- Eurocode:  $F_v = F_{\text{Johansen}} + F_{ax}/4$

# Density 1

- Well established that strength of fasteners depend on timber density
- Characteristic densities in EN 338 decrease rapidly with decreasing strength class:

C30	C24	C18	C14
380 kg/m <sup>3</sup>	350 kg/m <sup>3</sup>	320 kg/m <sup>3</sup>	290 kg/m <sup>3</sup>

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- Densities below 350 kg/m<sup>3</sup> very hard to find
- Up to now 350 kg/m<sup>3</sup> has been presupposed for all strength classes in Denmark
- C18 is most widely used in Denmark – loses 10 % of density

# Density 2

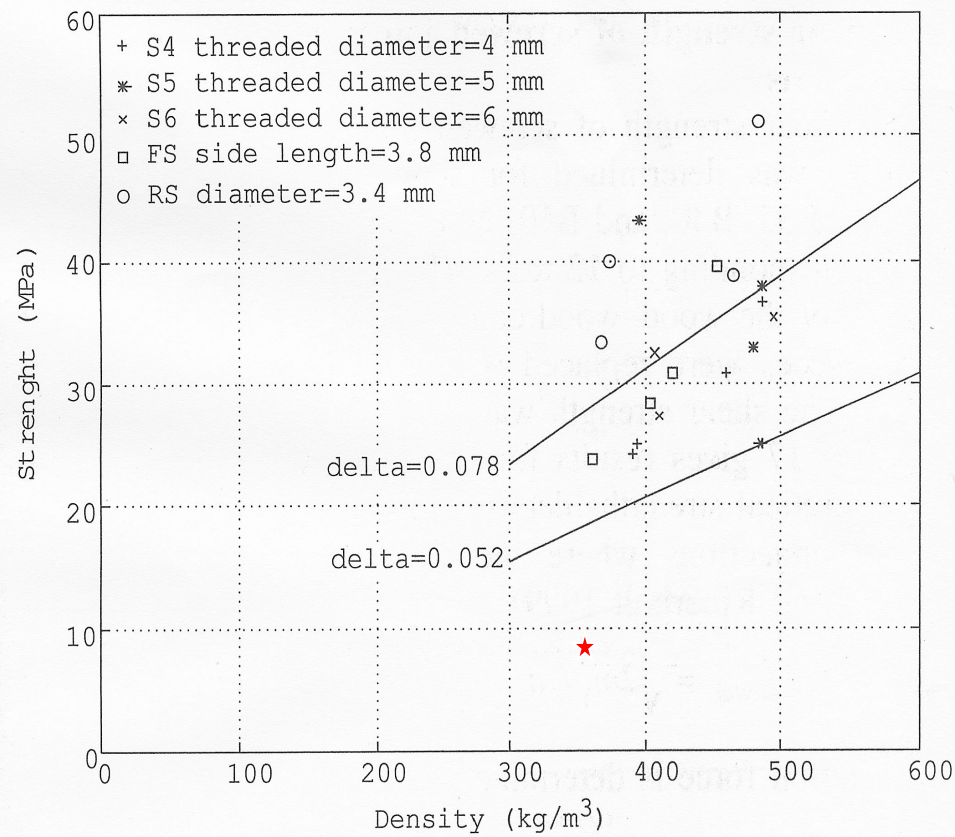
- Strength class for Nordic timber is usually governed by knot sizes – not the clear wood properties
- This might explain why the experience using 350 kg/m<sup>3</sup> is good
- If different grow conditions causes other relations for timber grown in other places EN 338 ought to take account of regional differences

# Axially loaded fasteners

- Head pull-through
- Withdrawal

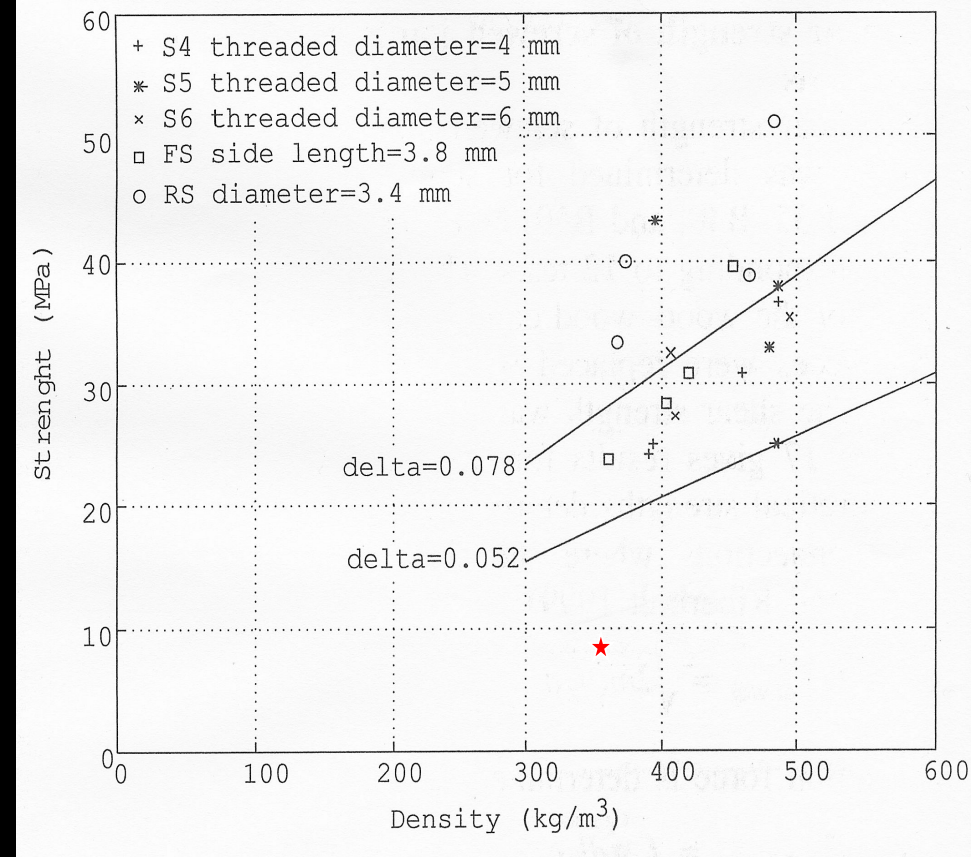
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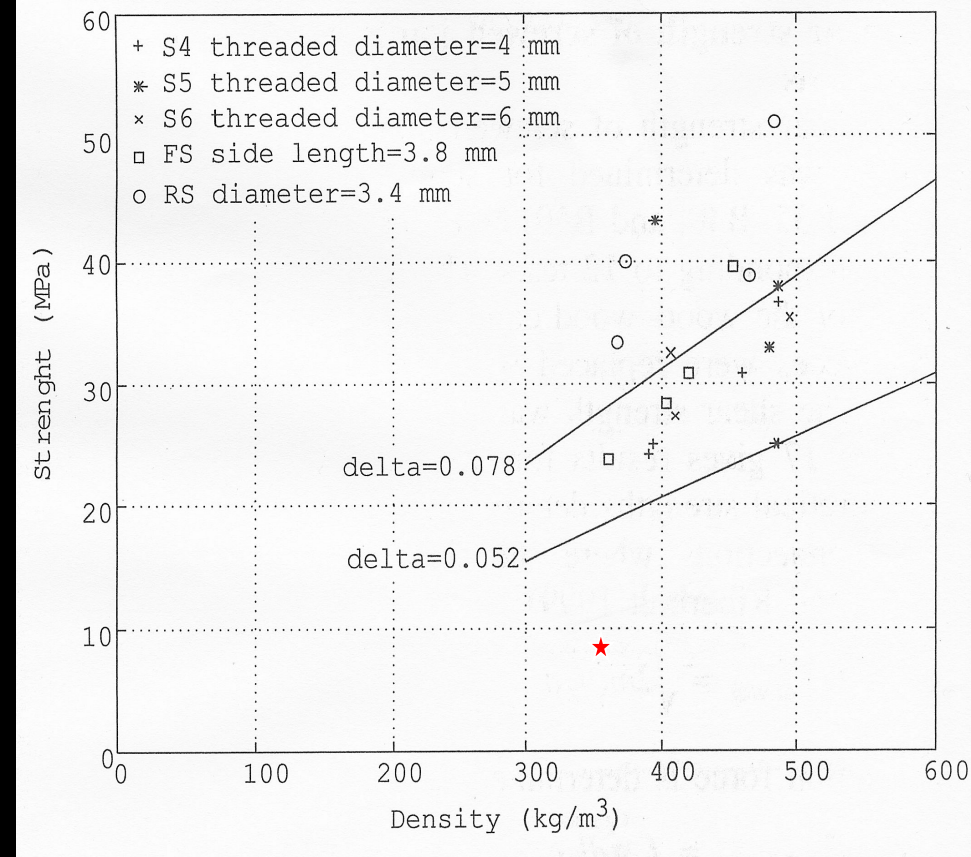
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- Nails: Depends on  $\rho^2$  !
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- A linear relationship appears reasonable for test values
- Correction from  $\rho = 350$  to  $\rho = 410$  with  $\rho^{0.8}$  makes only 3% difference from linear correction !



# Correction of measured strength for density

Example:

Head pull through, threaded nail,  $d_{\text{head}} = 5.5 \text{ mm}$

- $F_{\text{mean}} = 1500 \text{ N}$ ,  $\text{CoV} = 12.5\%$ ,  $\rho = 475 \text{ kg/m}^3$
- $f_{k,475} \sim 0.75 \cdot 1500 / 5.5^2 = 36,4 \text{ MPa}$
- Approved institute corrects to  $\rho = 350 \text{ kg/m}^3$  assuming linear relationship:

$$f_{k,350} = 26.8 \text{ MPa} (\sim 3 \times \text{EC5 for smooth nail})$$

- Using EC5's  $\rho^2$ -dependency unsafe for high  $\rho$
- Correction must be done with  $\rho^2$ :

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- Correction must be done with  $\rho^2$ :
- $f_{k,350} = 19.8 \text{ MPa} (\sim 2.3 \times \text{EC5 for smooth nail})$
- Preferable to use timber with smaller density for tests
  - or a range of densities including low densities

# Withdrawal – smooth nails

- Strength parameters given are NOT conservative!
  - especially not for round nails
- No difference in EC5 between round and square nails
- Reduction factor  $2/3$  for timber near to saturation not enough according to old Danish tests, might be  $1/3$

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- High withdrawal strength for smooth nail encourage the use of smooth nails for fastening of eg. roof battens
  - which might cause wind storm damage

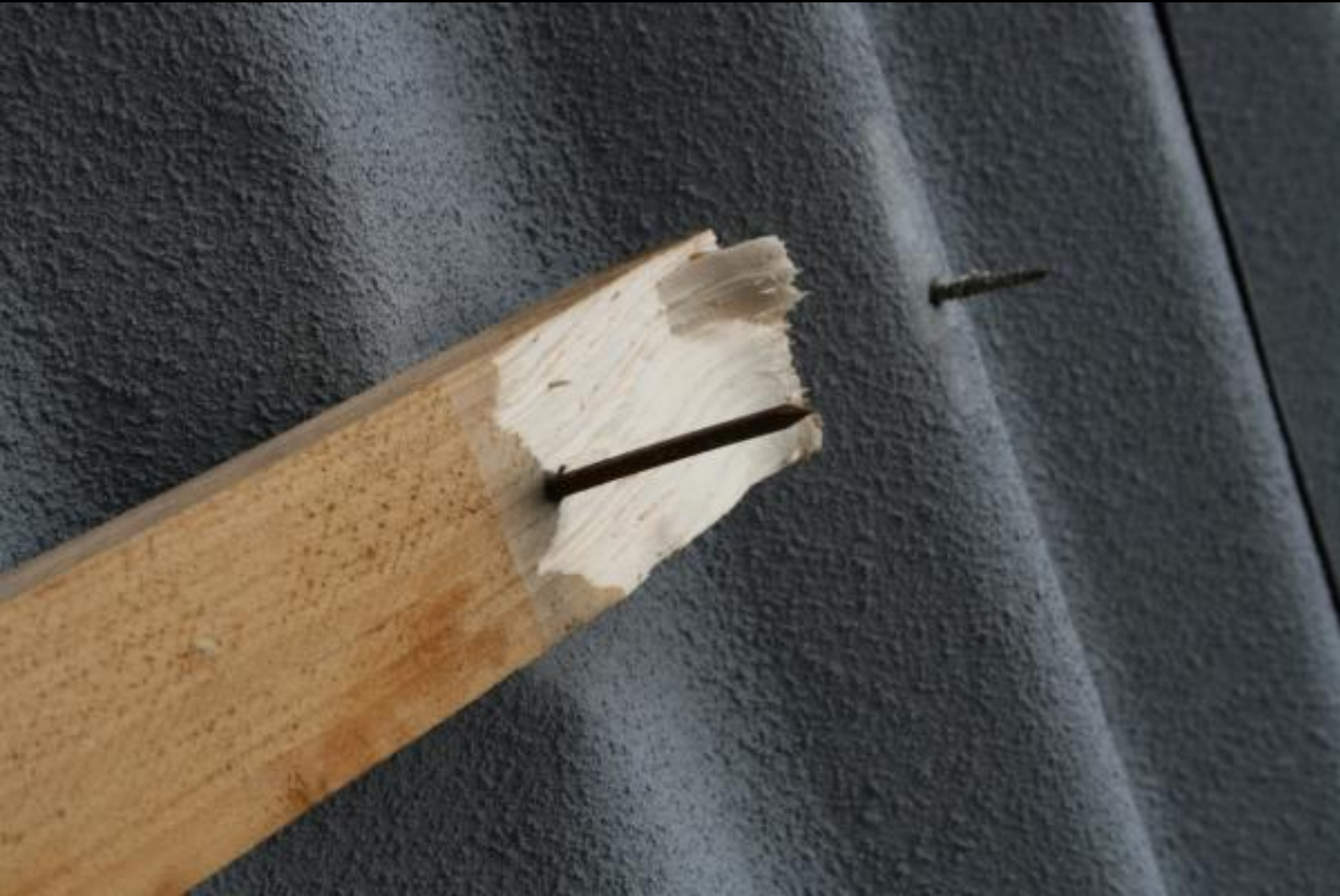
# Roof of steel plates

- 300 m<sup>2</sup> blew off
- Wind speed far from characteristic
- Other part of the roof blew off 3 years ago
- No strengthening considered!



# Cause

- Battens fastened with smooth nails (square and rusty)





# Withdrawal – threaded nails

- Strength parameter must be declared individually
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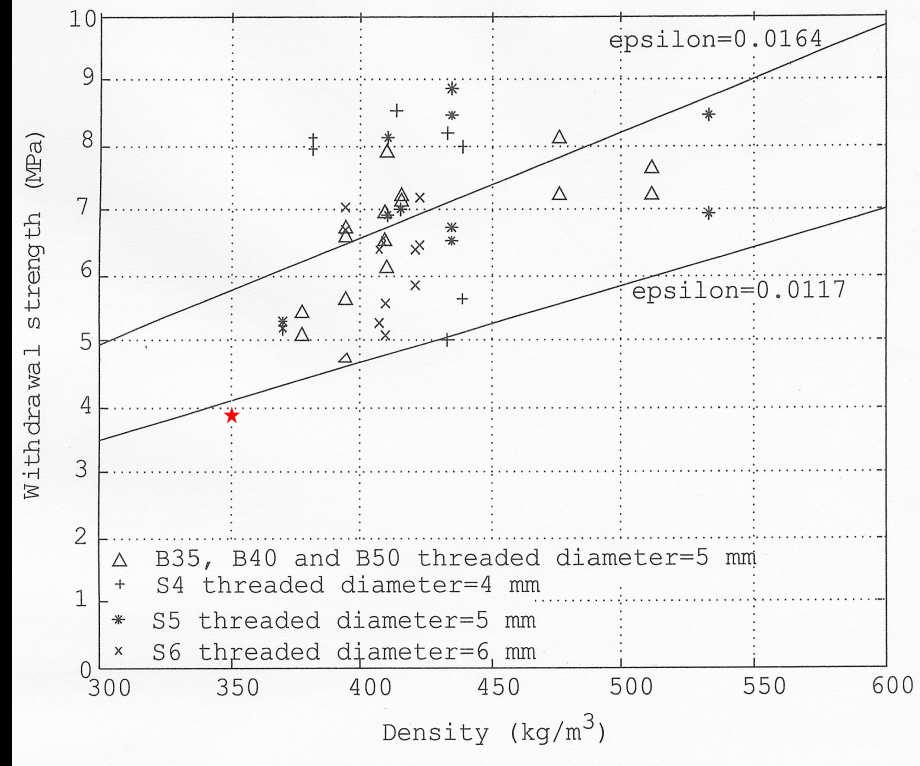
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- Danish code has  $5d + \text{point}$

# Withdrawal – screws 1

- Very complicated formula given and only for “old fashioned” screws with  $d = 6-12$  mm
- The simple formula  $0.035 d \ell_{\text{pen}} \rho$  can replace within 10% for  $d = 6-10$  mm
- ITT will give a single strength parameter, independent on e.g. length. A possible diameter dependency will be included in declared parameter
- Separate spacing requirements for withdrawal and only for timber thickness  $12d$  (which members thickness?)

# Withdrawal – screws 2

- No significant dependency on diameter for  $d = 4-6$  mm
- Connector screws and modern wood screws similar
- Fits well with (simplified) Eurocode formula



# Laterally loaded fasteners

- Nails, timber to timber
- Screws, timber to timber
- Steel to timber

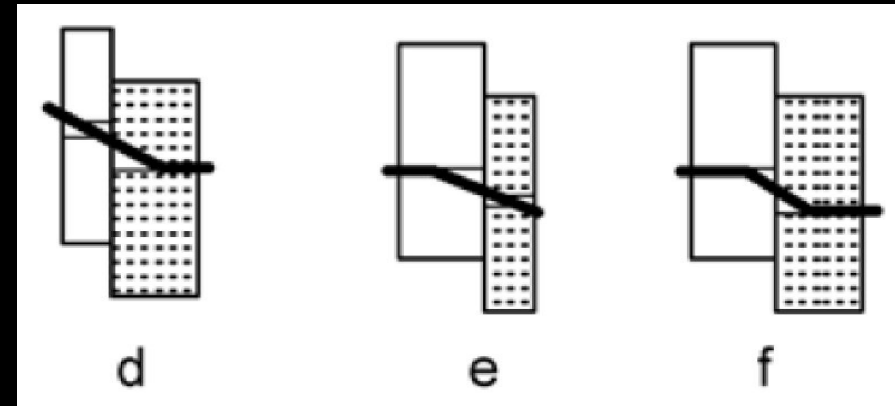
# Laterally loaded nails – timber to timber

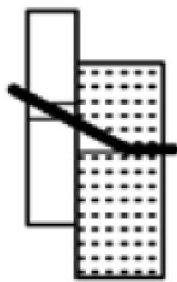
## Eurocode:

- Dowel load capacity from Johansen-theory with embedment strength and yield moment of fastener
- Rope-effect from friction and inclination

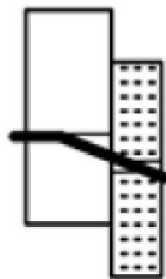
## Danish code:

- Presupposes failure-mode f
  - mode e not possible due to required penetration length
  - mode d somewhat prevented by the head
- Rope-effect included by reduced penetration length for threaded nails

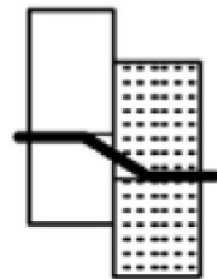




d



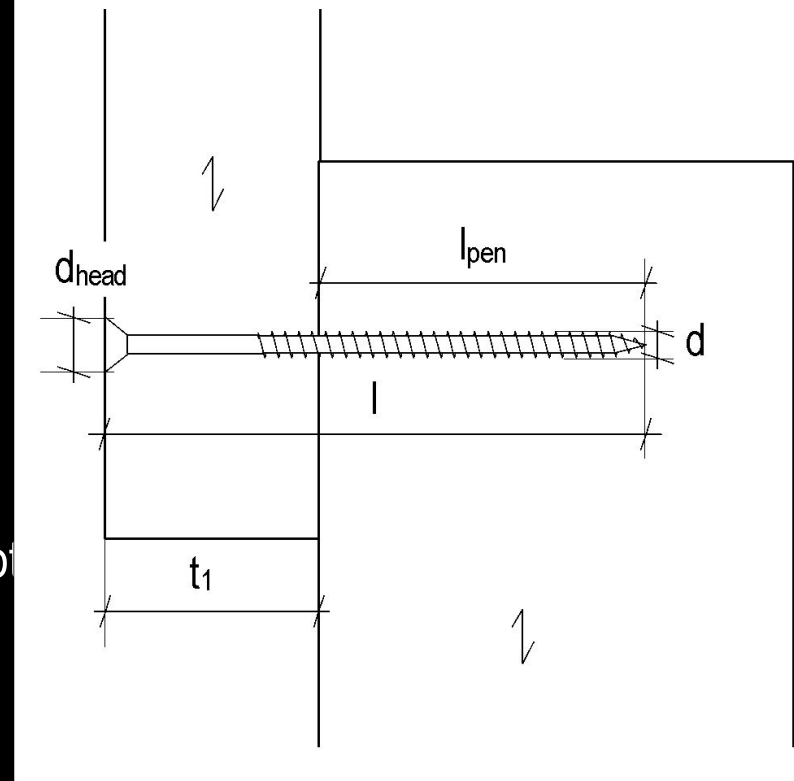
e



f

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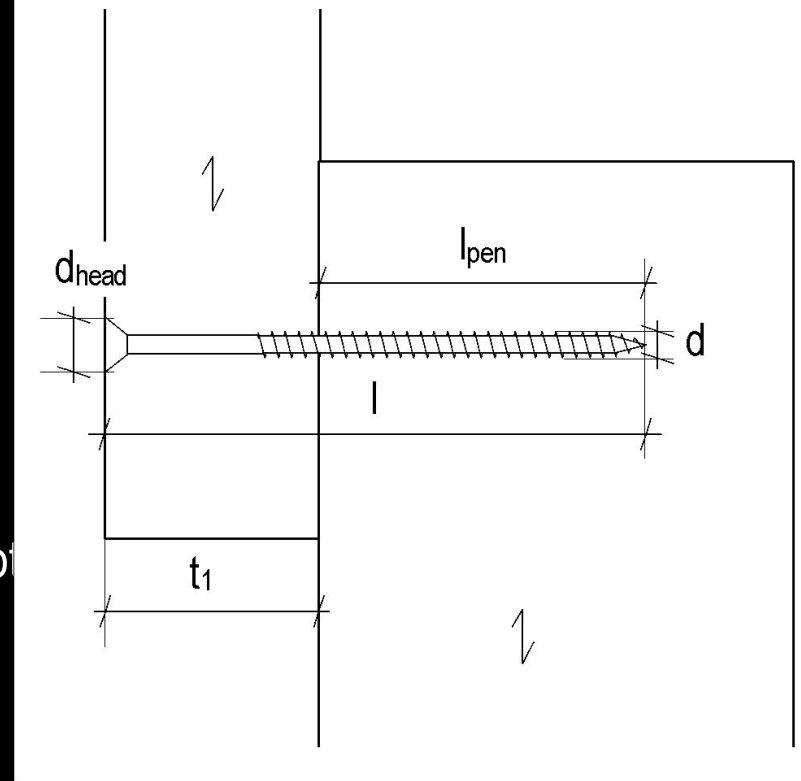
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- Eurocode suggests  $d_{\text{eff}} = 1.1 \times d_{\text{root}}$  for the threaded part of screws





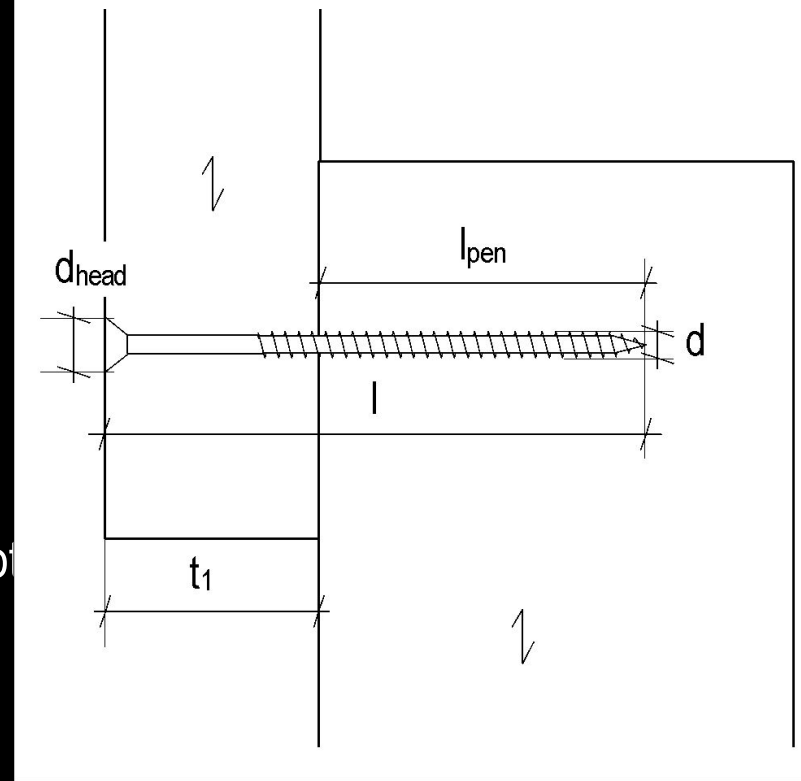
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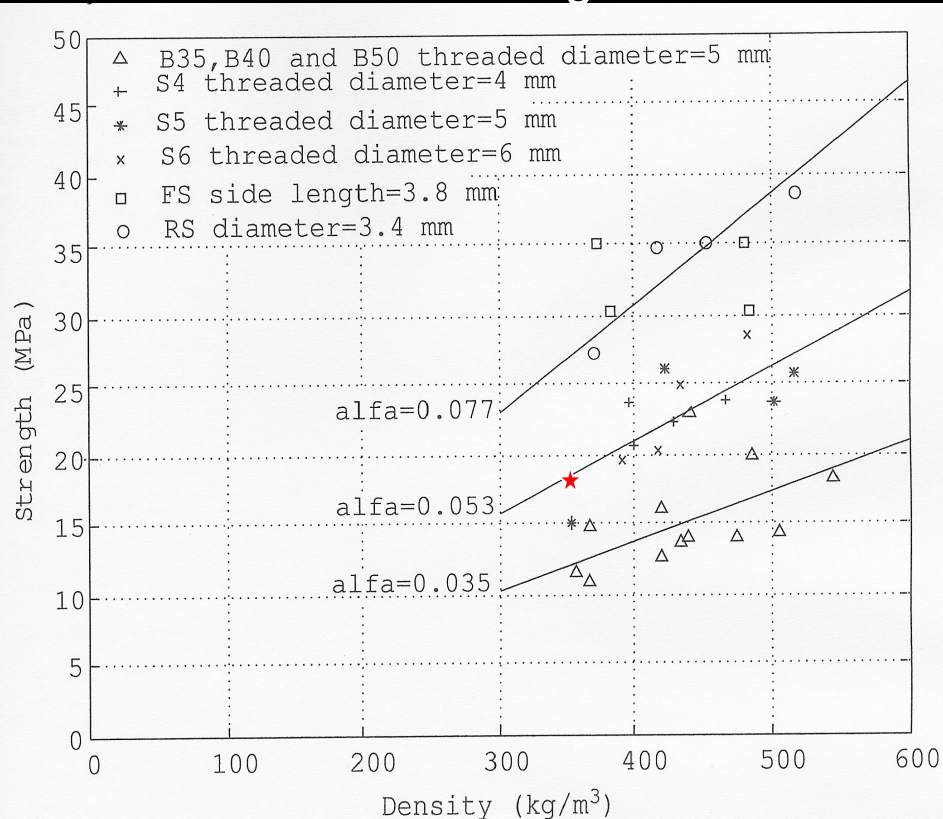
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- prEN 14592 does not deal with neither  $d_{\text{eff}}$  nor  $f_h$
- Most straight forward to declare  $f_h$  (for diameter  $d$ ) and  $M_y$



# Measured embedment strength for screws

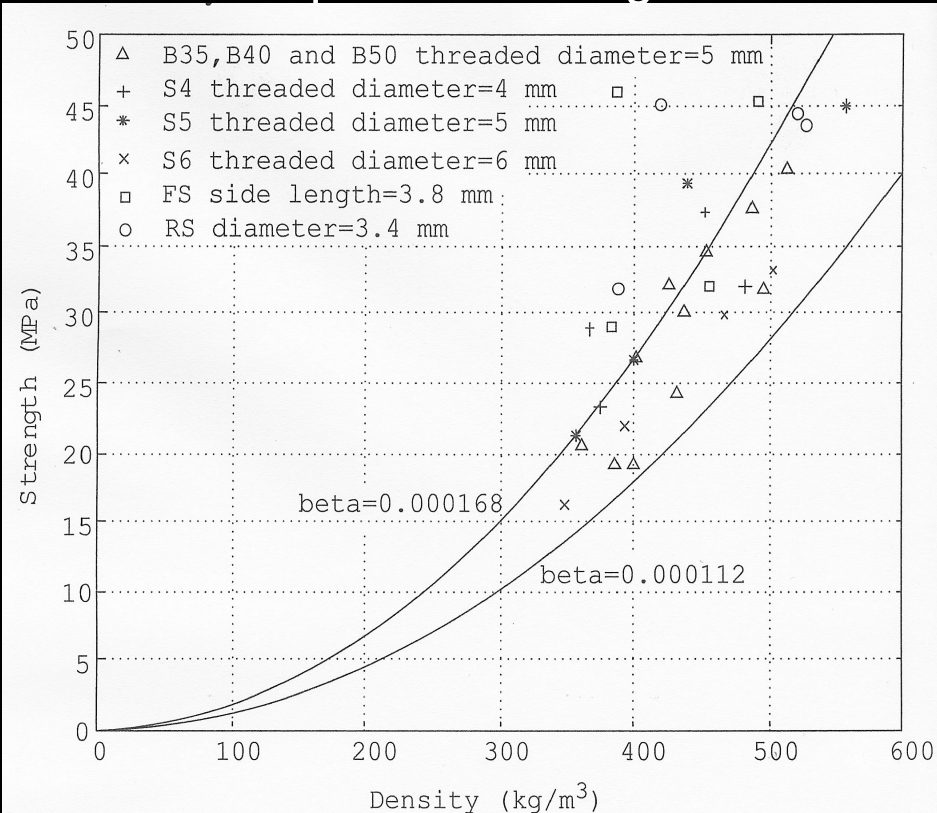
- $d_{\text{root}} / d \sim 0.6 \Rightarrow d_{\text{eff}} = 1.1 \times d_{\text{root}} = 0.66 d$
- Measured reduction factor for screws 0.45 – 0.7
- Hansen assumes factor to depend on surface roughness

Parallel to grain



<

Perpendicular to grain



# Laterally loaded nails - steel to timber

## Eurocode:

- Separate formulas for thick and thin steel-plates (head fixed against rotation or not)
- Thick plate  $t \geq d$ , thin plate  $t \leq d/2$

## Danish code:

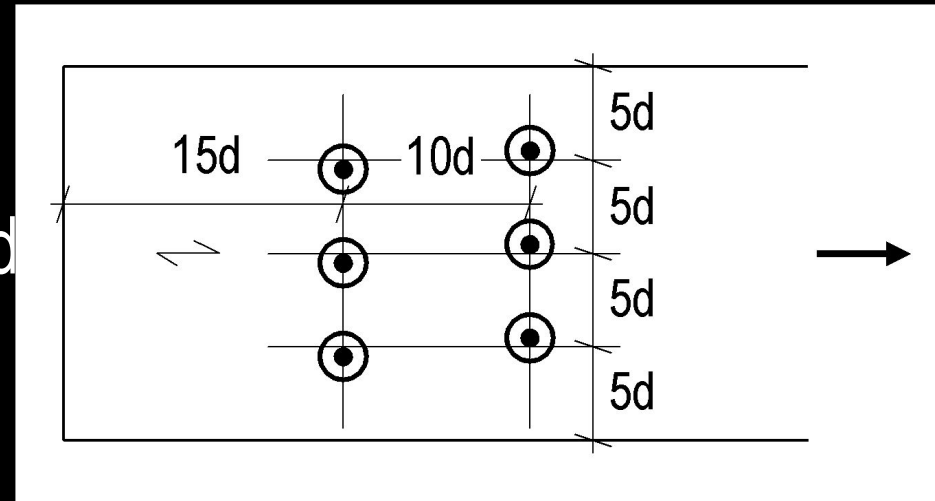
- Head assumed fixed against rotation
- Typical  $d = 4$  mm and  $t = 2$  mm
- Timber to timber strength increased by 25 % (larger rope-effect when not pull-through)

**TRZE**

Higher values will appear in an ETA-agreement for most commonly used connector nails and screws (smaller penetration length, larger rope-effect, fixed head)

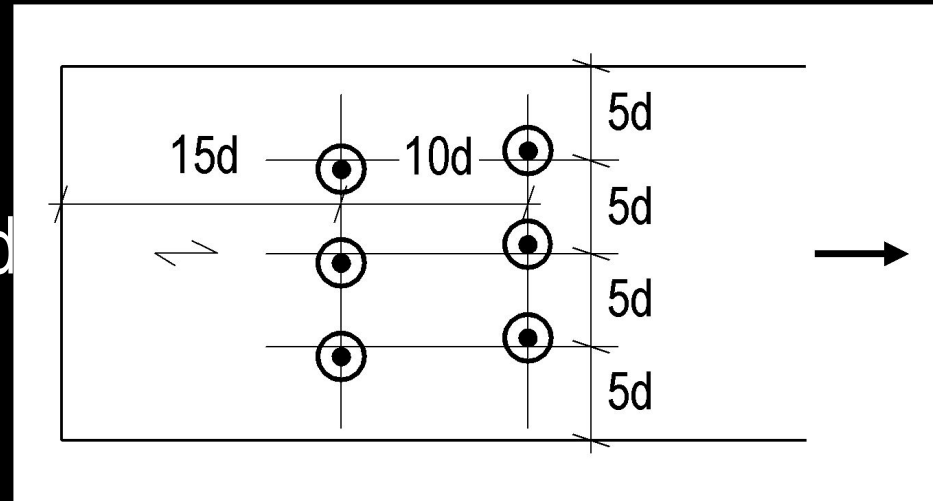
# Spacing parallel to grain

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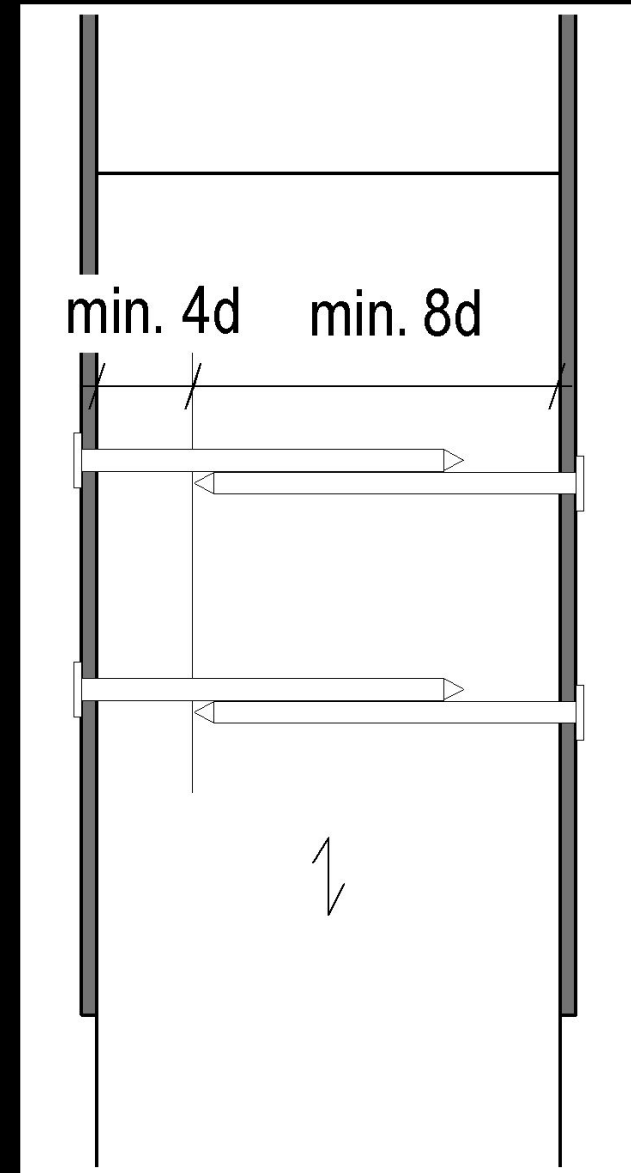
## Steel connector plates:

- Spacing can be reduced by factor 0.7
- Not possible to stagger
- Not specified if increased spacing requirement can be reduced by 0.7
- Very questionable if staggering is meaningful for small diameters



# Common connection not allowed by EC5

- 45 mm member with connector-plates on both sides
- Eurocode requires 4d from point to opposite site  
Minimum member thickens for  $d = 4$  mm:  
 $(4 + 8)d = 48$  mm
- Danish code requires only 3d from point to opposite site



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- For types of fasteners covered by Eurocode 5 the strength parameters are **mostly** - but not always - conservative
- The dependency on density should in general be similar for nails and screws
- Strict rules are needed for correcting measured strength parameters for density
- Preferable to carry out tests with a natural span of densities rather than a fixed density

# Conclusions 2

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- For screws **either** embedment strength for diameter of thread **or** effective diameter should be a declared parameter
- Spacing requirement in grain direction unnecessary and unclear for connector plates
- Replacing the Danish timber code with Eurocode 5 reduces the load capacities of most fasteners significantly
- Rules for two-sided nailing a catastrophe for Danish construction